



上海交通大學

SHANGHAI JIAO TONG UNIVERSITY

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# Thermodynamic and kinetic characteristics of composite sorbents and their multi-mode sorption heat storage

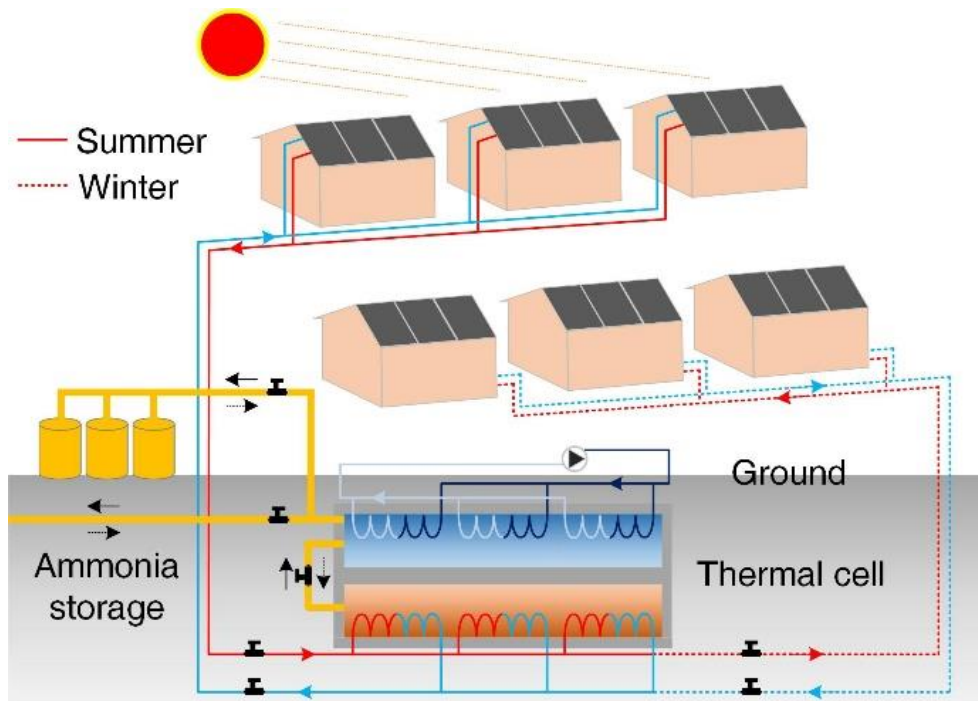
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Reporter: Guoliang An

Adviser: Liwei Wang

October 8, 2020

## Thermal energy storage



Long-term thermal energy storage

- Storage density (material, system)
- Storage grade (material, cycle)
- Heat loss (material, structure)
- Heat adaptability (material, cycle)

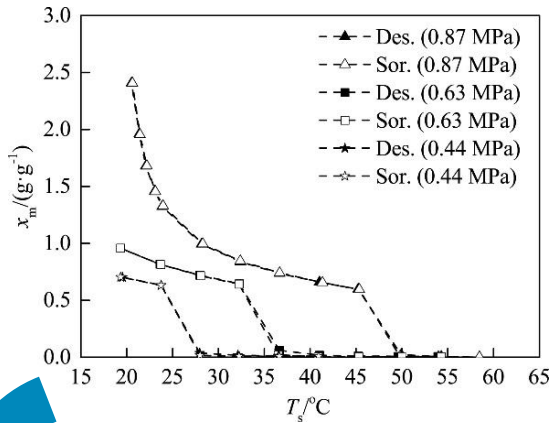
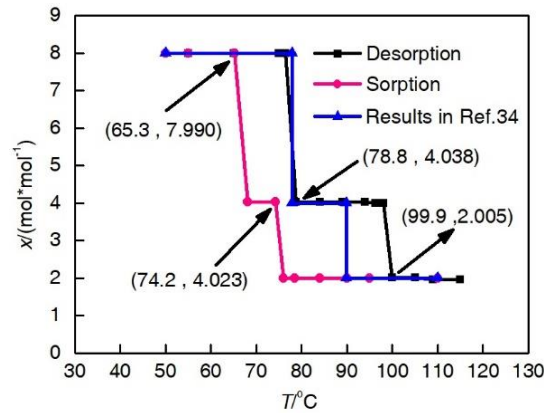
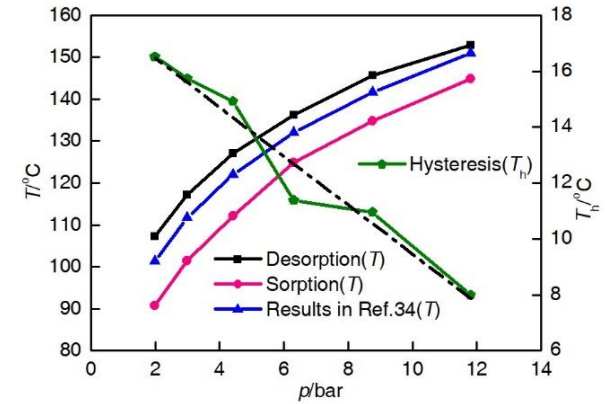
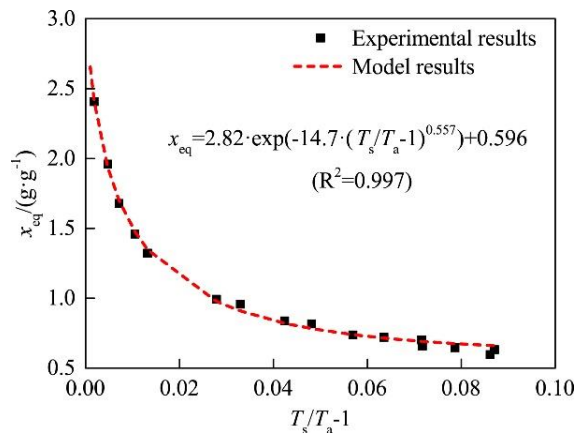
## Comparison between thermal energy storage

Storage	Sensible	Latent	Sorption
Density	Low	Middle	High
Grade	Decline	No decline	Decline
Loss	Large	Large	Almost none
adaptability	Good	Not good	Not good

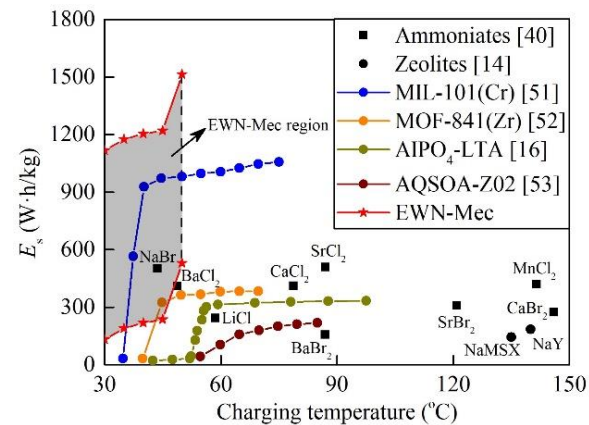
Target:

- 1 Slow down the decline of sorption thermal energy storage (STES) grade
- 2 Improve the heat source adaptability of STES

## Halide/ENG-TSA

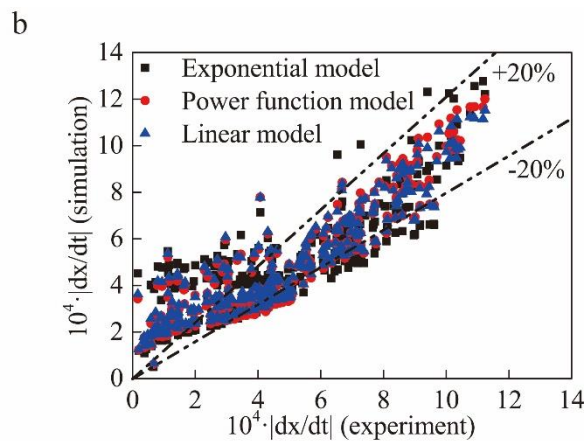
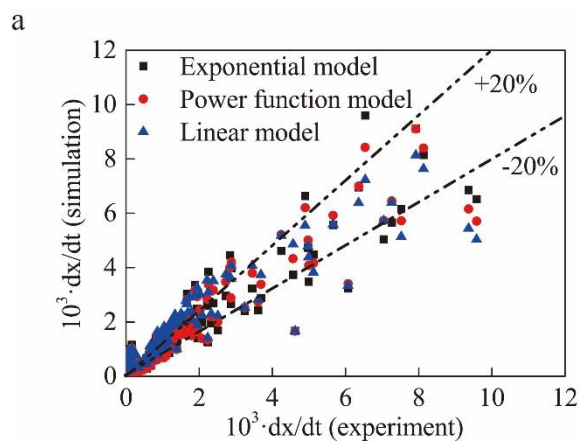
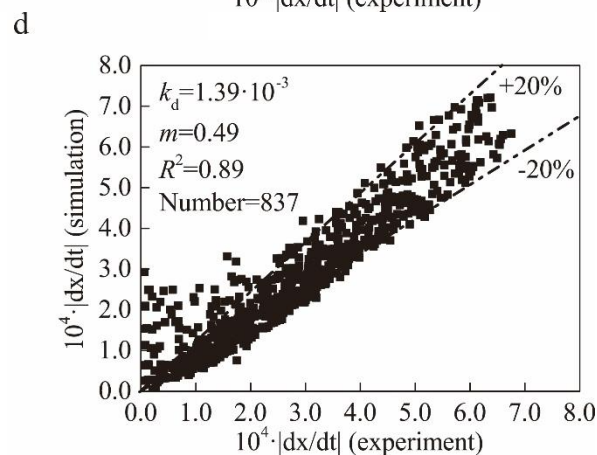
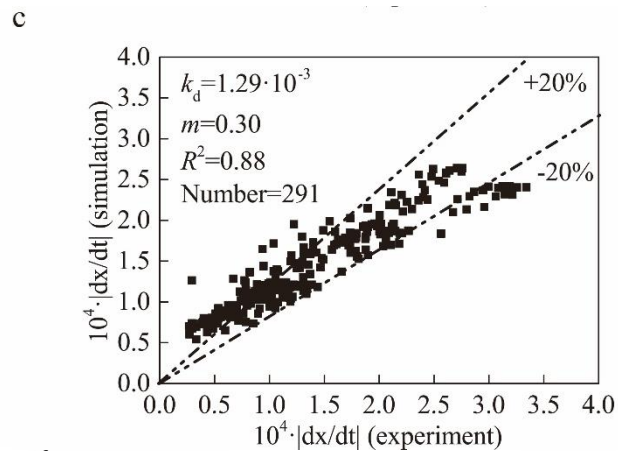
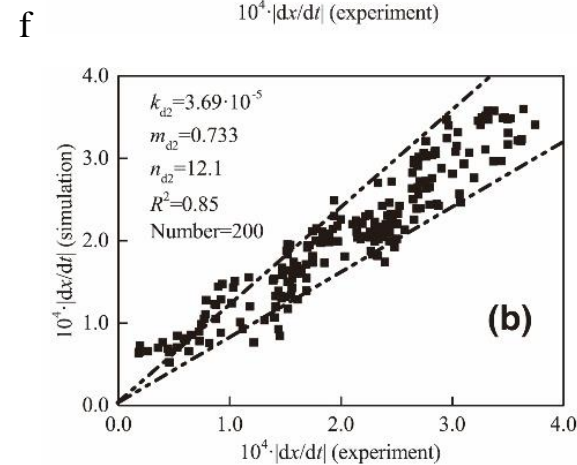
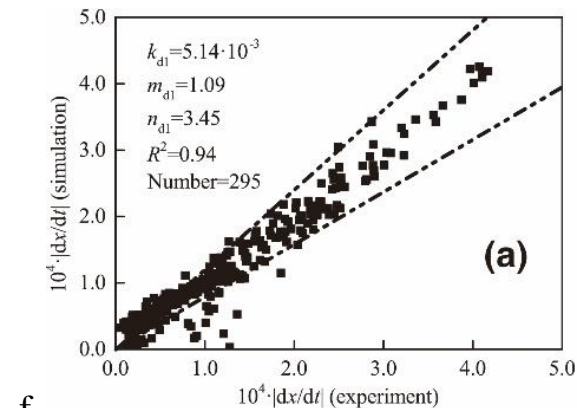
 $\text{NH}_4\text{Cl}$  $\text{CaCl}_2$  $\text{MnCl}_2$ 

Thermodynamics model



Storage density

## Model selection

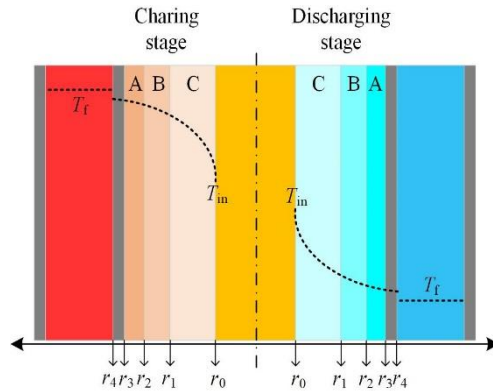
MnCl<sub>2</sub>CaCl<sub>2</sub>NH<sub>4</sub>Cl

## Parameter results

Reaction	Analogical model	Range
Mn <sub>2-6</sub>	$\frac{dX}{dt} = 1.19 \cdot 10^{-2} \left(1 - \frac{p_{eq}(T_s)}{p_c}\right) (1-X)^{0.64}$	$X \in (0, 1)$
Mn <sub>6-2</sub>	$\frac{dX}{dt} = -2.08 \cdot 10^{-3} \left(\frac{p_{eq}(T_s)}{p_c} - 1\right) X^{0.36}$	$X \in (1, 0)$
Ca <sub>2-4</sub>	$\frac{dX}{dt} = 2.14 \cdot 10^{-3} \left(1 - \frac{p_{eq}(T_s)}{p_c}\right) (1-3X)^{0.17}$	$X \in (0, 1/3)$
Ca <sub>4-8</sub>	$\frac{dX}{dt} = 2.6 \cdot 10^{-3} \left(1 - \frac{p_{eq}(T_s)}{p_c}\right) \left(\frac{3}{2} - \frac{3}{2}X\right)^{0.50}$	$X \in (1/3, 1)$
Ca <sub>8-4</sub>	$\frac{dX}{dt} = -9.27 \cdot 10^{-4} \left(\frac{p_{eq}(T_s)}{p_c} - 1\right) \left(\frac{3}{2}X - \frac{1}{2}\right)^{0.49}$	$X \in (1, 1/3)$
Ca <sub>4-2</sub>	$\frac{dX}{dt} = -4.30 \cdot 10^{-4} \left(\frac{p_{eq}(T_s)}{p_c} - 1\right) (3X)^{0.30}$	$X \in (1/3, 0)$
NH <sub>4 0-max</sub>	$\frac{dx_m}{dt} = 6.41 \cdot 10^{-3} [x_{eq}(T_s) - x_m(T_s)]^{0.648} \cdot \left(1 - \frac{p_{eq}(T_s)}{p_c}\right)^{1.55}$	$T_s < T_c$
	0	$T_s > T_c$
NH <sub>4 max-0</sub>	$\frac{dx_m}{dt} = -5.14 \cdot 10^{-3} [x_m(T_s) - x_{eq}(T_s)]^{1.09} \cdot \left(\frac{p_{eq}(T_s)}{p_c}\right)^{3.45}$	$T_s < T_c$
	$\frac{dx_m}{dt} = -3.69 \cdot 10^{-5} [x_m(T_s) - 0]^{0.733} \cdot \left(\frac{p_{eq}(T_s)}{p_c}\right)^{12.1}$	$T_s > T_c$

Material  
kineticsHeat/mass  
transferReactor  
model

## Model verification

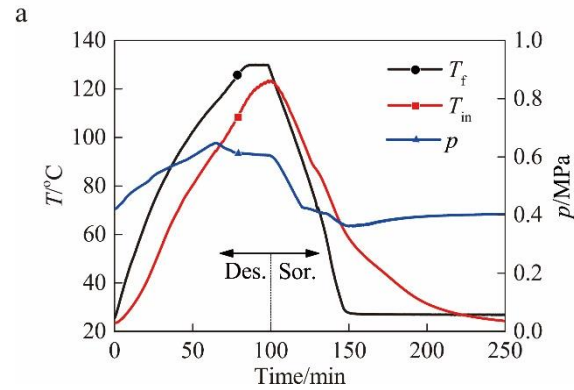


Reactor model

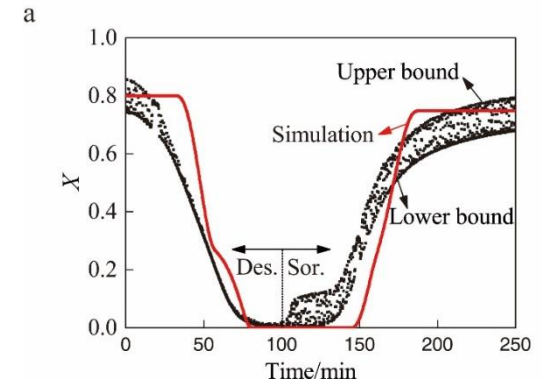
$$\rho c \frac{\partial T}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left( \lambda r \frac{\partial T}{\partial r} \right) + S$$

$$\frac{\partial T}{\partial r} \Big|_{r=r_0} = 0$$

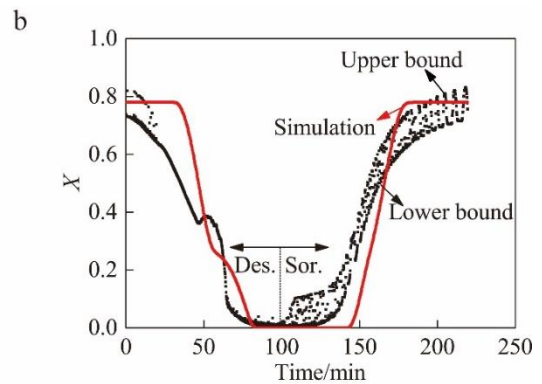
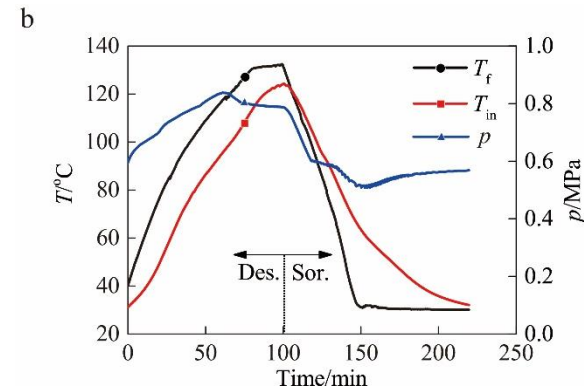
$$h_f (T_{f\_in} - T \Big|_{r=r_4}) = \lambda \frac{\partial T}{\partial r} \Big|_{r=r_4}$$



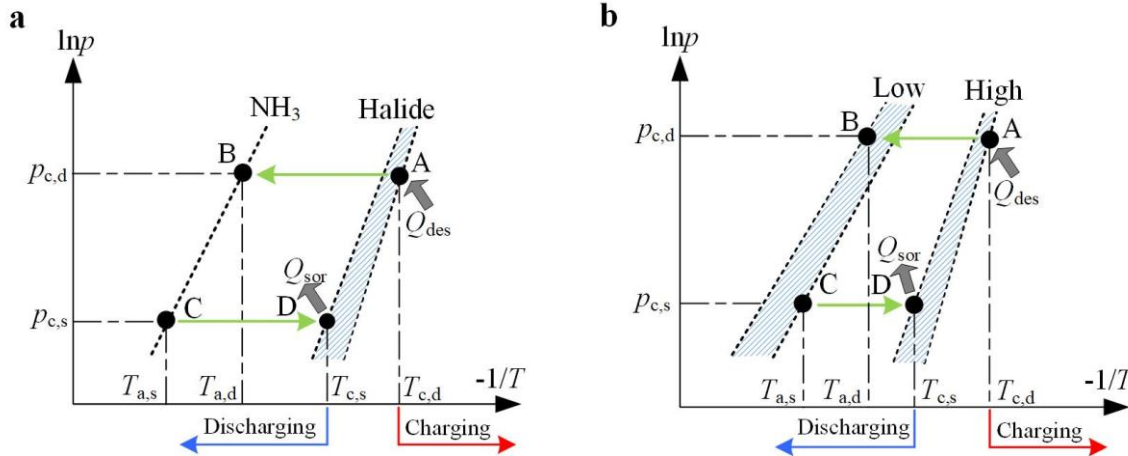
Temperature



Sorption capacity



## Cycle evaluation



Single/multi-halide

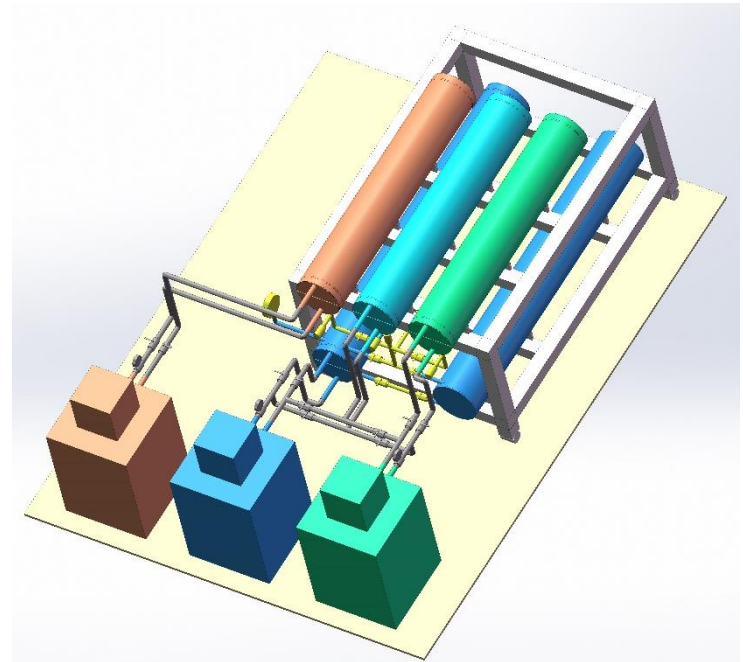
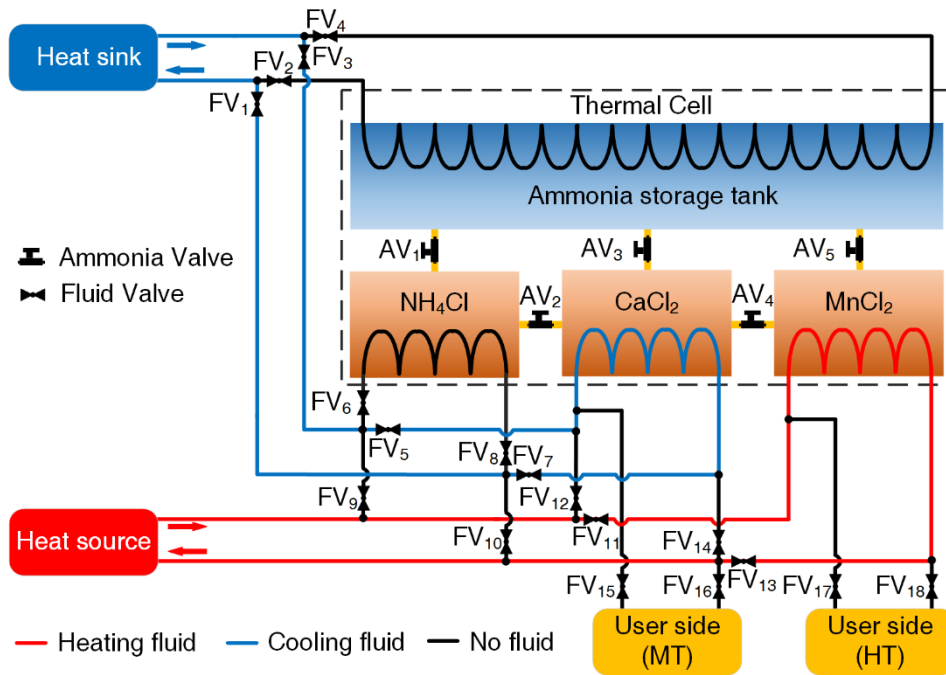
Sorption/resorption

Short/long term storage

$T_{f, in} (^{\circ}\text{C})$	50	60	70	80	90	100	110	120	130	140	150	160	170	180
$E_{s, dis} \text{ (short)}$	NH <sub>4</sub>				NH <sub>4</sub> -Ca		Ca							
$E_{s, dis} \text{ (long)}$	NH <sub>4</sub>				NH <sub>4</sub> -Ca		Ca							
$t_{dis} \text{ (short)}$	NH <sub>4</sub>													
$t_{dis} \text{ (long)}$	NH <sub>4</sub>													
$\Delta T_f \text{ (short)}$	NH <sub>4</sub> -Mn	Ca-Mn	NH <sub>4</sub> -Mn	Ca	Mn	NH <sub>4</sub> -Mn			Mn					
$\Delta T_f \text{ (long)}$	NH <sub>4</sub>		NH <sub>4</sub> -Ca		Ca				NH <sub>4</sub> -Mn		Mn			
$\Delta E_{dis} \text{ (short)}$	NH <sub>4</sub>				NH <sub>4</sub> -Ca		Ca							
$\Delta E_{dis} \text{ (long)}$	NH <sub>4</sub>				NH <sub>4</sub> -Ca		Ca							
ECOP (short)	Mn		NH <sub>4</sub>											
ECOP (long)	NH <sub>4</sub>		NH <sub>4</sub>											



## System construction



Based on two-stage cascading desorption cycle



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Thanks for your attention

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